# Direct current (DC) supply grids for LED-Lighting

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## Abstract

Most electrical devices operate on direct current (DC) internally, but are supplied by alternating current (AC). A power supply with DC makes the rectifier electronics unnecessary. This makes the devices simpler and more reliable and generates less power losses. Especially, if many identical devices like lamps in supermarkets or open offices are operated, this becomes evident.

This publication aims to show solutions of DC operated professional buildings like offices or supermarkets and homes. A special focus is put on high voltage supply at 380 Vdc. First, the component effort for solutions with AC and DC current supply are compared. Especially LED-lamps can benefit from a DC supply, because lamp drivers can be reduced to a few reliable components. Then, a loss breakdown including transmission losses is presented. The major advantage of a DC supply appears, if a micro- grid including decentralized energy generation and storage is considered. In addition, standardization initiatives working on high voltage DC grids are listed. Finally, a realized office test bed including DC light emitting diode (LED) illumination and photovoltaic (PV) support is presented.

## 1. Introduction

One trend in lighting is to distribute light sources. This becomes possible with LED lamps, which offer small but efficient light power. However, this also requires efficient lamp drivers. Furthermore assigning each lamp its individual lamp driver becomes a high effort in material. Therefore, concepts are needed to deal with such an increased number of similar lamp drivers. One solution could be to use a DC power supply. This allows omitting the rectifier electronics, which makes the devices simpler, more reliable and generates less power losses. This is attractive especially in installations, where a high number of lamps are connected to a power rail like in open space offices or supermarkets (see Figure 1). Each lamp contains an AC to DC conversion circuit, which can be omitted with a DC supply rail. This becomes especially attractive, if the system is combined with a local photovoltaic generator, as shown in [1].

DC supply systems are proposed by a number of publications especially for residential applications, e.g. [2] [3]. But as derived e.g. in [4], a large variety of different requirements for different devices, a DC system for residential applications faces even larger challenges. Contrary, in lighting applications the loads are quite similar in their requirements and thus much better suited for a common DC supply.

This publication gives an overview of the opportunities of using a DC grid in professional and home buildings. They are demonstrated on a realized installation of an office building DC lamp system with PV support at Philips Research, Eindhoven



Figure 1: Lamp installations in open office space (a) and supermarkets (b).

## 2. Effort for AC to DC conversion

Figure 2 shows the block diagram of a typical lamp driver operated on AC with the parts necessary for AC to DC conversion. Similar components are necessary for all AC power supplies.

The rectifier is the essential element and is typically a bridge rectifier consisting of four diodes. The electrolytic capacitor (elcap) levels out the pulsating rectified sinusoidal voltage. Recently IEC SC77A WG1 agreed to a new review of the standard IEC 61000-3-2, which means that in the near future lamp drivers with more than 5 W will require a power factor correction (PFC) circuit. A PFC ensures that the current drawn from the grid is sinusoidal. The PFC may consist of an inductor, but this is usually too bulky. Especially for higher power levels a switch mode converter, typically a step up converter (boost converter), is used. However, this requires a filter to avoid higher frequency content generated by the switched mode PFC polluting the grid.

#### 2.1. Space and components saving

Figure 3 shows a photograph of a Philips Xitanium lamp driver for a 39 W light emitting diode (LED) lamp as used in the reference setup (see later chapter 5). In the figure, all parts, which are necessary for AC to DC conversion, are marked. As can be seen, approximately 40% of the printed circuit board (PCB) is occupied by these components. Especially the PFC and the filter circuit require a lot of space. The storage elcap is also significant, but the bridge rectifier itself is a comparable small component.

As now discussed, these components might also be necessary for DC operation. An overview of this is shown in Table 1. The bridge rectifier may be necessary to allow an arbitrary connection of the DC supply leads. However, this problem may also be solved by a suitable mechanical coding of the plug to avoid a wrong connection. The elcap may be needed to suppress voltage dips of the DC supply. However, it should be acceptable for lamps to pass the dips to the lamp and allow a short flicker. Then, an elcap is not necessary.

If the DC supply voltage has a large variation, it may be necessary to convert it to a constant level of an intermediate voltage. This requires a DC to DC converter, similar to an active PFC. However, if the DC voltage range has a narrow specification, such a DC to DC converter can be omitted.

The filter is necessary to suppress high frequency contents of switched mode converters. It becomes necessary, if an active PFC is used. If the lamp driver itself uses switched mode conversion, it remains necessary. However, with a linear lamp driver, even the filter may be omitted.

Concluding, the components needed for AC to DC con-version can be omitted if the DC power plug is mechanically coded, if dips can be accepted, if the voltage is specified in a narrow range and, optional, if a linear lamp driver is used.



Figure 2: Typical AC lamp driver.



Figure 3: Power driver for a 35 W LED lamp.

Table 1: Overview of required components for AC to DC conversion.

Component	AC supply	DC wide voltage range and reverse polarity protection	DC narrow voltage range, mechanical rev. polarity protection
Filter	Required because of PFC	Required because of DC-DC	Can be omitted with linear driver
Rectifier	Required	Required for reverse polarity	Omitted
Power factor correction (PFC) / DC-DC converter	Required for P > 25W	Required to match wide voltage range	Not necessary
Elcap storage	Required to avoid flickering	Required because of dips	Can be omitted, if dips are accepted

## 2.2. Linear LED driver

The advantage of a lighting DC supply becomes most obvious with LED lamps. A most simple "driver" for a LED is simply a resistor. If the supply voltage is very well defined, this would be the most simple, reliable and durable "lamp driver". However, if the voltage is less stable, the brightness of the LED would vary remarkably, because a small voltage variation already leads to large change of the output power.

A nearly as simple solution is a linear current driver. Such a linear current source can easily be built with one J-FET and one resistor. Such a circuit may exhibit a good efficiency. The efficiency of such a circuit is calculated assuming a constant forward voltage  $U_d$  of the LED and neglecting a residual voltage drop at the FET. The results are presented in Figure 4. As long as the DC supply voltage  $U_s$  is larger than the forward voltage  $U_d$ , the LED power (blue) is the nominal value. If the supply voltage increases above  $U_d$ , the voltage across the FET rises linear. The power loss in the FET (orange) increases proportional to it. From the LED power and the losses the efficiency (yellow) is calculated.

If the voltage variation is within  $\pm 10\%$  around the nominal voltage  $U_N$  (like in the public AC grid as well), the efficiency can still be above 84%. This simple and reliable circuit can thus achieve an efficiency, which is similar to small switched mode converters, as long as the voltage range is narrow enough.



Figure 4: Power and loss characteristic of a linear current controlled LED driver

## 2.3. Loss savings

The components needed for AC to DC conversion also generate losses. Typically, the smaller the device is, the lower is the efficiency. Own measurements showed losses in the order of 5% of the output power for lamp drivers. This arrangement is shown in Figure 5a. These losses can be saved, if the device is operated on DC. However, if the DC grid is supplied from the AC grid, a central rectifier is needed in addition. However, this central rectifier can be more efficient due to its larger size. Its losses are estimated to about 2% of its output power, as illustrated in Figure 5b. In addition, cable losses can be reduced, if a DC voltage

of 380 V is used, as shown in Figure 7 (chapter 3). In total, losses of about 5% of the output power could be avoided using a 380 V DC grid.



Figure 5: Loss comparison of AC grid (a) and DC grid (b).

Even larger loss savings can be achieved in a different use case as illustrated in Figure 6. It shows a system, which is optimized for self-consumption of photovoltaic (PV) energy. The PV energy harvested during the day is stored in a battery storage and used in the evening.

If all components are connected to the AC grid, losses in the AC to DC (and vice versa) converters end up to 10% to 13% of the output power (see Figure 6a). In a DC system, these losses can be completely avoided (see Figure 7b). Reference [5] shows a similar result for such a system, where operation including PV and battery is considered.



Figure 6: Loss comparison of AC grid (a) and DC grid (b) with photovoltaic and battery storage operation.

## 3. Voltage selection

The supply voltage of the DC grid also has an influence on the losses. Low voltages like 24 V or 48 V have as advantages that they are save to touch and commercially available devices exist. However, to transmit the same power, much higher current *I* is necessary compared to 230 V AC. A high DC voltage like 380 V is compatible to many 230 V AC devices, which operate on a similar intermediate DC voltage internally.

The power loss  $P_{loss}$  in the cable is proportional to the square of the current *I*:  $P_{loss} \sim I^2$ . Figure 7 shows the cable losses which appear at different supply voltages, scaled to the losses at 230 V AC. To achieve the same losses at higher currents, the cable cross sectional area *A* must be also scaled proportional to the current:  $A \sim I^2$ . Therefore, the same Figure 7 shows the amount of copper, which is necessary to achieve the same losses as with the 230 V AC supply.

It is clearly seen that the low voltages of 24 V and 48 V either generate extremely higher losses or require significant more copper. It also shows that a 380 V DC supply generates only about 1/3 of the losses compared to 230 V AC. It should be noted that insulation properties of 230 V AC cables are also suitable for 380 V DC operation, because they need to withstand the peak voltage.

This safety issue is discussed with other safety issues more in detail in reference [6]. It concludes that operating at a DC voltage of less than 380 Vdc can be considered as similar as operating at 230 Vac. A further safety aspect of DC grids discussed is arcing, which especially appears, when a load is unplugged during operation. Therefore, it must be take care of not exchanging lamps during operation in a DC system.



Figure 7: Comparison of cables losses for different supply systems. Losses are scaled to 230 Vac. Cable losses are equivalent to copper effort, if similar losses are achieved. *Remark:* 380 Vdc requires similar insulation as 230 Vac.

#### 4 Standardization on 380 V DC

The voltage level of 380 V DC is not only attractive for lighting applications, but also for other applications like the power supply in data centers. Most advantage will be available, if the DC supply system is standardized. Several organizations work on the standardization. Table 2 gives an overview of the organizations and their current work.

Organization	Торіс	
International Electrotechnical Commission (IEC)	Many standards covering low voltage DC grid systems already SMB SG4 working group "LVDC distribution systems up to 1500V DC":	
	Managing new standardization projects at IEC technical committees (TC)	
	National standardization working groups. Germany: TBINK-LVDC working group at DKE/VDE	
European Telecommunication Standardisation Institute (ETSI)	European Standard: EN 300 132-3-1 V2.1.1 (2012-02)	
	Value: Definition of DC appliance inrush current limits and measurement setup	
EMerge Alliance	Standardization working group on 380 V DC power grids for datacenters	
Allance	Standardization working group on 380 V DC for campus and microgrids	

Table 2: Overview of organizations working on standardization of low voltage DC grids.

#### **5 DC lighting demonstration setup**

To demonstrate the functionality and to experience the problems related to it, a DC lighting demonstration is set-up in an office building at Philips Research in Eindhoven, The Netherlands. Figure 8 shows a schematic overview of the system.

The DC part operates on 380 Vdc and consists of a rectifier, a 2 kWpk photovoltaic (PV) generator and 54 LED lamps with 37 W each. The lamps are driven by lamp drivers, which are adapted to the DC system. Figure 9 shows photographs of the PV panels and of some of the lamps. The lamps illuminate the floor and are switched on during the whole working hours at daytime. In the best case, the PV generator is able to supply all the DC lamps. No feed in of PV power into the AC grid is provided. The lamps are Philips Xitanium lamps, with drivers modified for DC operation.

For reference, a 230 V AC system is also in operation. Here, the PV power is directly fed into the mains grid. Furthermore, 18 comparable AC operated Xitanium LED lamps are monitored.



Figure 8: DC-grid demo installation with solar support and ac reference grid. Grid Voltage: 380 Vdc, Solar Modules: 2 kWpk, LED Lamps: 56 x 37 W, adapted LED drivers, Reference system: 230 Vac.



Figure 9: Photos of the reference system: Photovoltaic panels (left), LED-Lamps (right).

In the DC system, beside others the energy drawn from the mains grid is monitored. In the reference AC system, the energy needed by the lamps (including drivers) and the energy generated by the photovoltaic system (grid feed in) is monitored. To get a comparison, the needed lamp energy in the AC system is scaled to the number of lamps in the DC system, the generated PV energy in the AC system is scaled to the size of the DC PV system and finally both values are subtracted to achieve a net energy demand comparable to the DC system. Data was measured from 29.April 2013 until 6. Sept. 2013. From the monitored energy the average power was calculated. The results are shown for the DC power demand and the scaled AC power demand in figure 10. There are two gaps in the data resulting from failures and maintenance time, which are not considered for the final comparison. The figure shows that the power demand of the DC system is always lower than that of the comparable AC system. In total, the DC system demand was 2132.6 kWh, while 2181.4 kWh relate to the scaled AC system. Concluding, the DC system energy demand was 2.24% lower than the comparable AC system.



Figure 10: Comparison of total consumption in the DC system and the AC reference system. The energy in the AC system is scaled to the DC system.

#### 7 Conclusion

Operating lamps and other devices with a residential DC grid offers two major benefits:

Overall power losses can be reduced. However, for a supply of the residential DC grid from a public AC grid, this effect is partly compensated by losses in the central rectifier. But energy savings become visible especially with the integration of additional local power sources.

As a further benefit, complexity can be reduced in the powered devices by shifting it into the infrastructure. This can make the devices more durable and reliable. Especially for mass products like lamp drivers and consumer devices, which are manufactured and used in a huge number, this will reduce the overall cost. From a system point of view, it is advantageous to make those devices, which are needed in a large number, as simple and cheap as possible and to allow a few central devices being more complex. This cost advantage should be considered as the main benefit of the DC system.

The specification of a DC system should take these benefits into account: To reduce losses in the distribution system, the voltage should be as high as possible. For lamps, an operating voltage like 380 V DC is proposed. To allow the reduction of complexity, especially the definition of a narrow voltage tolerance is required.

#### References

[1] Ulrich Boeke, Matthias Wendt, Lennart Yseboodt, "Combined Solar and AC Mains Powered LED Lighting System", 14th European Conference on Power Electronics and Applications (EPE'11), Birminham, United Kingdom, 30.Aug.-1.Sept.2011.

[2] T.-F. Wu, Y.-K. Chen, G.-R. Yu, Y.-C. Chang, "Design and Development of DC-Distributed System with Grid Connection for Residential Applications", 8th International Conference on Power Electronics - ECCE Asia, May 30-June 3, 2011, The Shilla Jeju, Korea, paper no. TuF1-4.

[3] Rakwichian Wattanapong, "Community Smart Grid for ASEAN Decentralize Power", Presentation at World Alternative Energy Forum, Chiang Mai, Thailand, 12.-14. Dec. 2012. (Online available (29.6.2014) at http://www.adicet.cmru.ac.th/waef2012/)

[4] Bernhard Scheeren, "Optionen für eine Gleichstromversorgung in einem Wohnhaus", Masterthesis at Cologne University of Applied Science, Institute for Electrical Power Engineering, Cologne, Germany and Zuyd Hogeschool, Heerlen, The Netherlands, 16. April 2014.

[5] Suponthana Wuthipong, "MW Scale Stand-Alone PV Hybrid Mini Grid System", Presentation at World Alternative Energy Forum, Chiang Mai, Thailand, 12.-14. Dec. 2012. (Online available (29.6.2014) at http://www.adicet.cmru.ac.th/waef2012/)

[6] Jung-Hoon Ahn, Dong-Hee Kim, Byoung-Kuk Lee, Hyun-Cheol Jin, Jae-Sun Shim, "DC Appliance Safety Standards Guideline through Comparative Analysis of AC and DC Supplied Home Appliances", Journal of Electrical Engineering & Technology Vol. 7, No. 1, 2012, pp. 51~57, Online available (29.6.2014) at: http://dx.doi.org/10.5370/JEET.2012.7.1.51